



Osawatomie, KS
Mitigation Planning Technical
Assistance

Pottawatomie Creek Flood Forecasting Using Lane Gage

February 14, 2020



Agenda

1 Introductions

2 Meeting Objectives

3 Project Review - Technical Memo

4 Results – Open Discussion



Introductions

FEMA Region VII

- Andy Megrail, GIS Project Manager
- Dawn Livingston, Risk Analyst

U.S. Army Corps of Engineers

- Allen Chestnut, Senior Hydrologic Engineer
- Jennifer Wood, Levee Safety Program Manager

Kansas Department of Agriculture-Div. of Water Resources

- Steve Samuelson, NFIP Coordinator
- Tara Lanzrath, Floodplain Mapping Coordinator
- Joanna Rohlf, Floodplain Mapping Specialist
- Bill Pace, Floodplain Mapping Specialist

Stantec

- Anish Pradhananga, Senior Engineer
- Chunyan Li, Engineer in Training
- Will Zung, Project Manager



Meeting Objectives

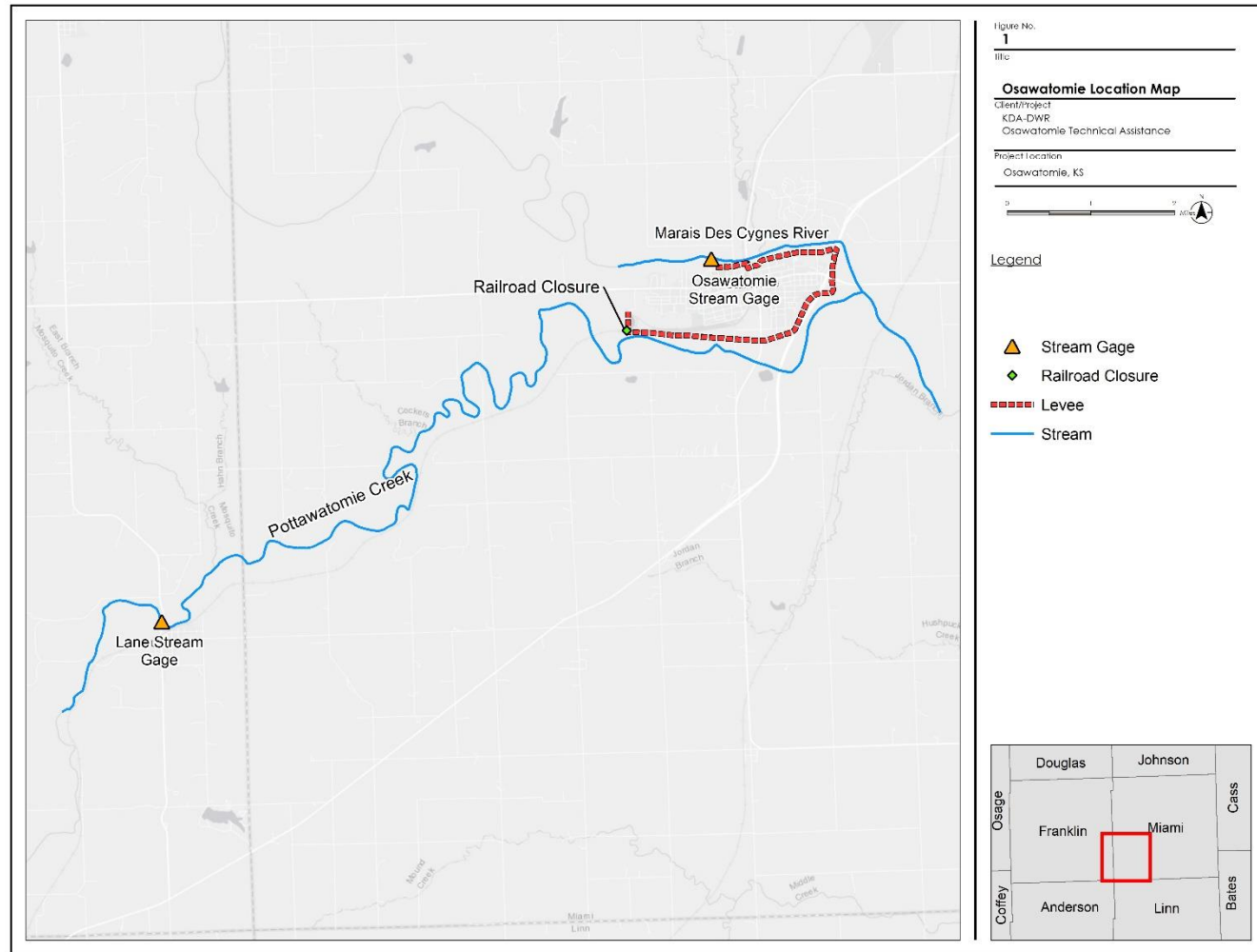
- Gain understanding of methodology of forecasting floods at locations downstream of gages.
- Have awareness of the hydrologic and hydraulic modeling applied for the flood forecasting at the levee.
- Understand the results in flood forecasting tables
- Understand how these tables combined with the stream gage forecasts can be used as reference for decisions by the city

Project Review

Technical Analysis

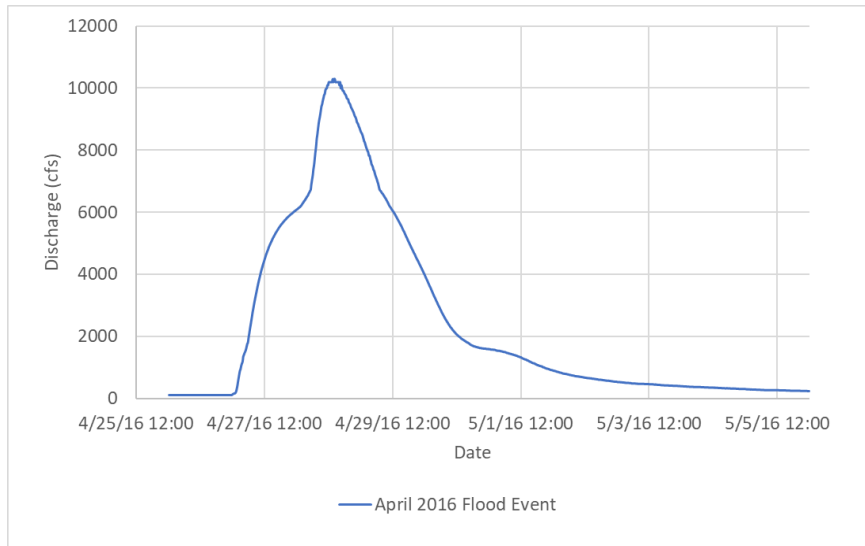
- Research Flood Forecasting Methodology
 - Flood Inundation Mapping (FIM) Program
 - Recommended Methodology
- Hydrologic Analysis
 - Hydrograph Development
- Hydraulic Analysis
 - Model Development
 - Model Calibration
- Flood Forecasting
 - Methodology

Technical Analysis – Study Area

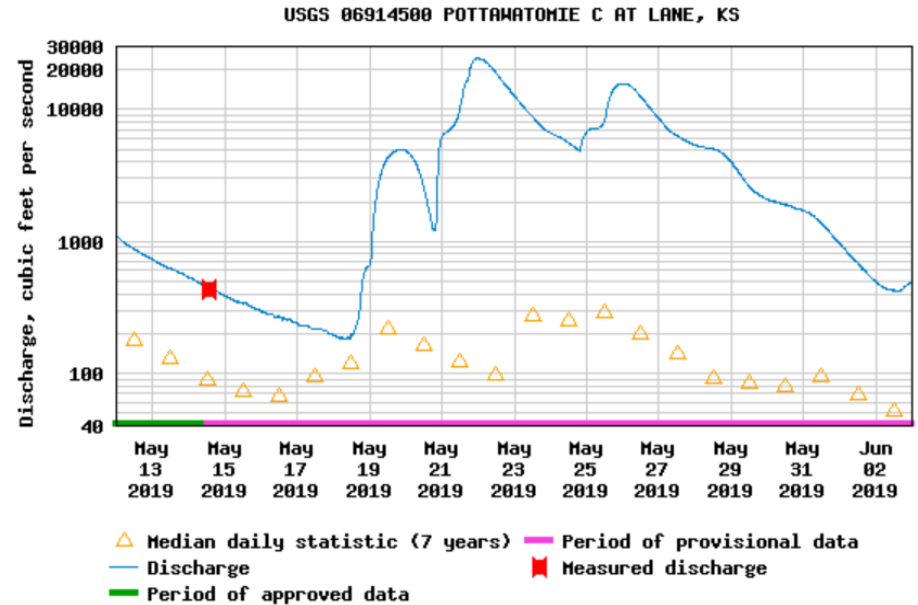


Technical Analysis – Hydrology

Pottawatomie Creek: USGS 06914500 at Lane, KS



April 2016 hydrograph

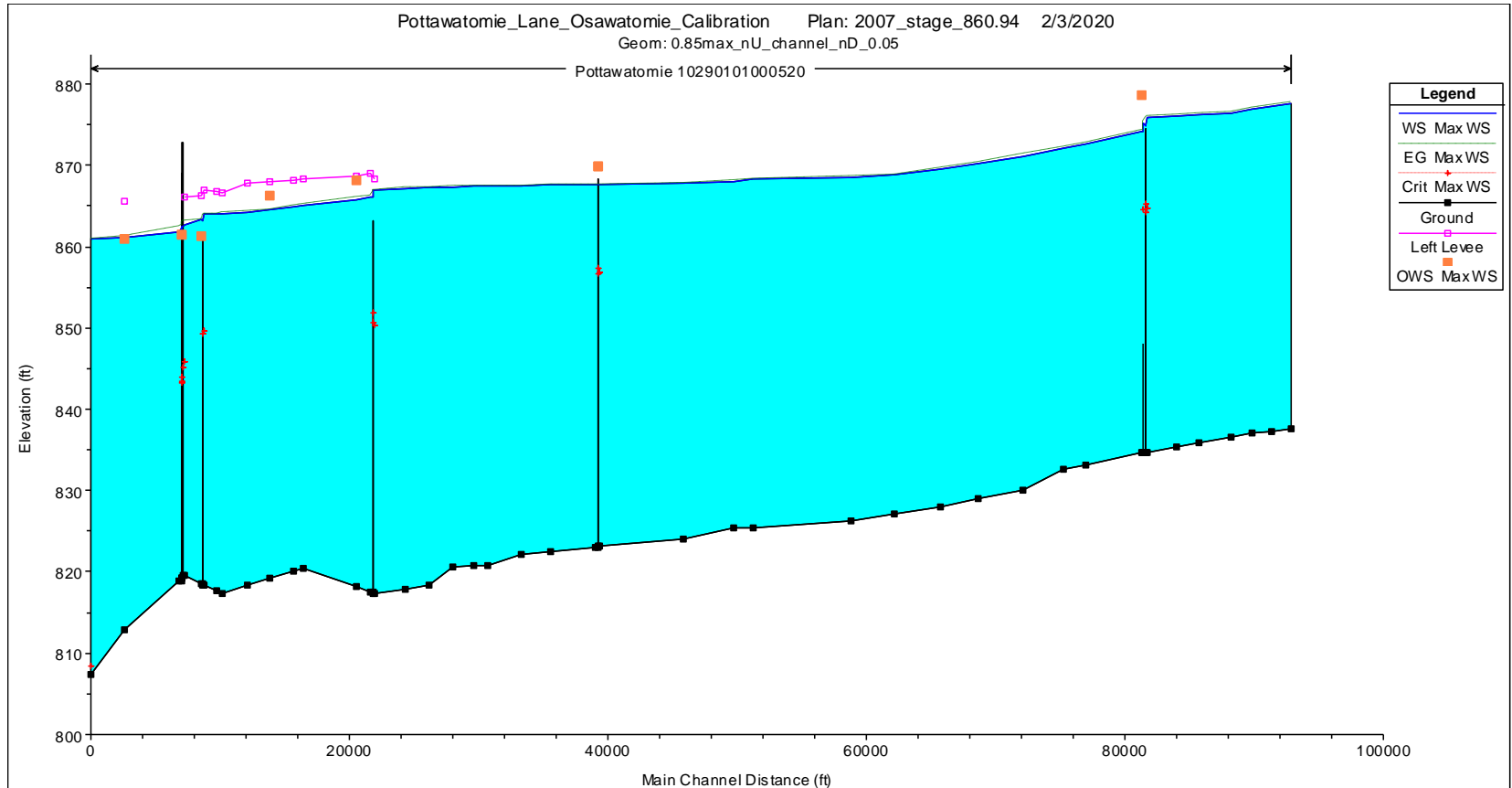


May 2019 hydrograph

Technical Analysis

Calibration to 2007 Flood Event-High Water Marks

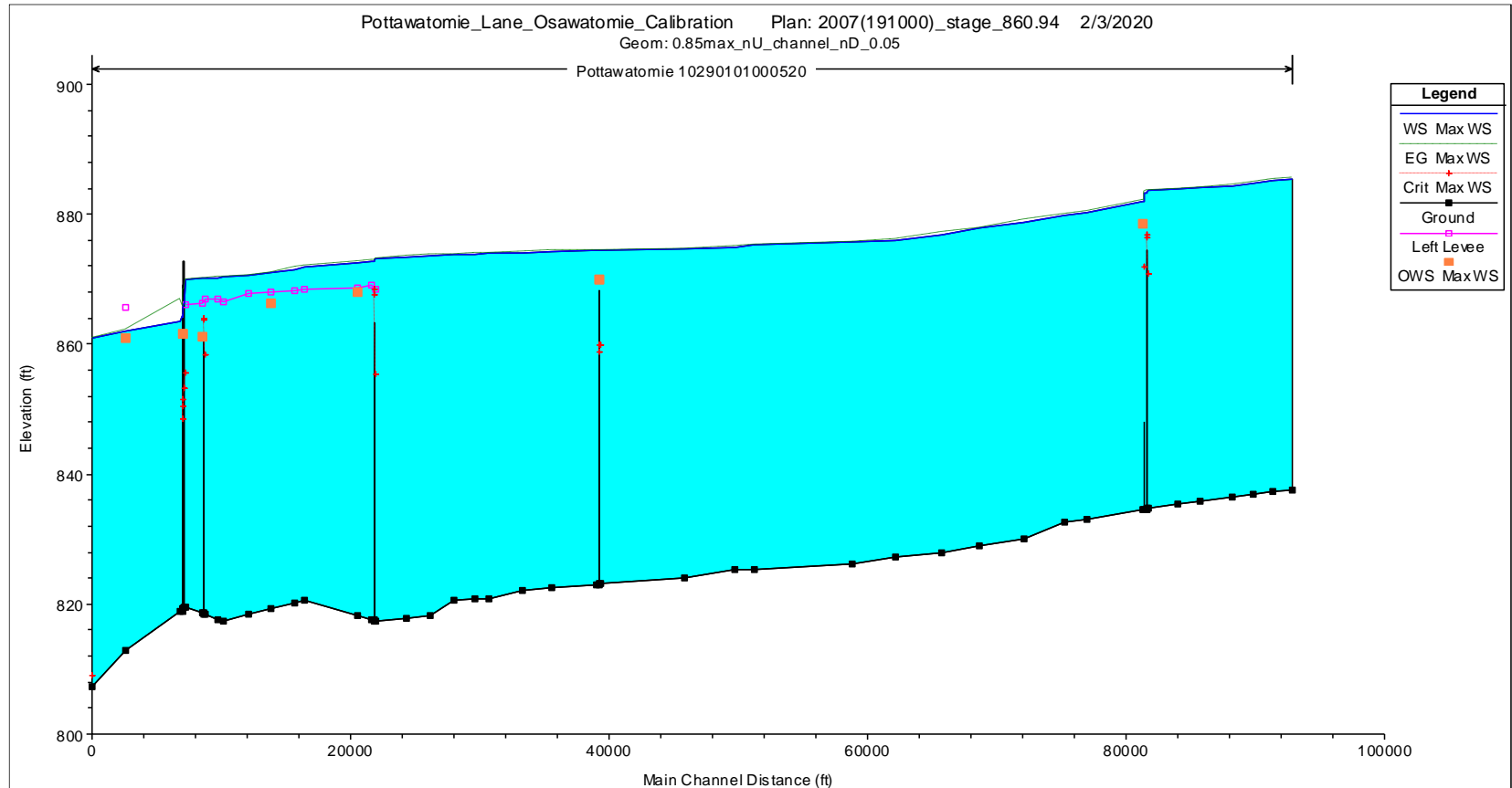
peak flow of 80,000 cfs, stage hydrograph of 860.94 ft BC



Technical Analysis

Calibration to 2007 Flood Event-High Water Marks

peak flow of 190,000 cfs, stage hydrograph of 860.94 ft BC



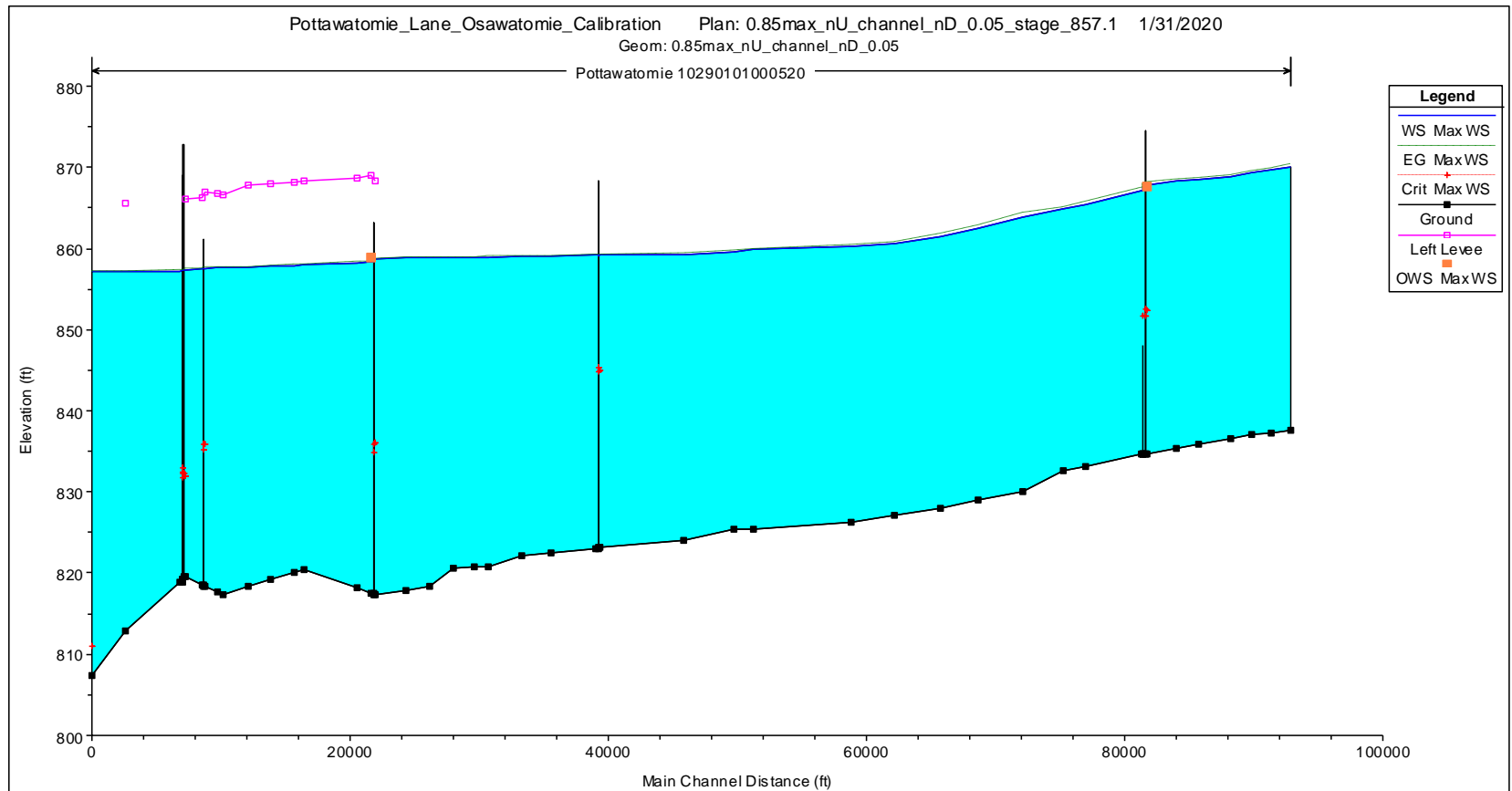
Technical Analysis

Calibration to May 2019 Flood Event



Technical Analysis

Calibration to May 2019 Flood Event



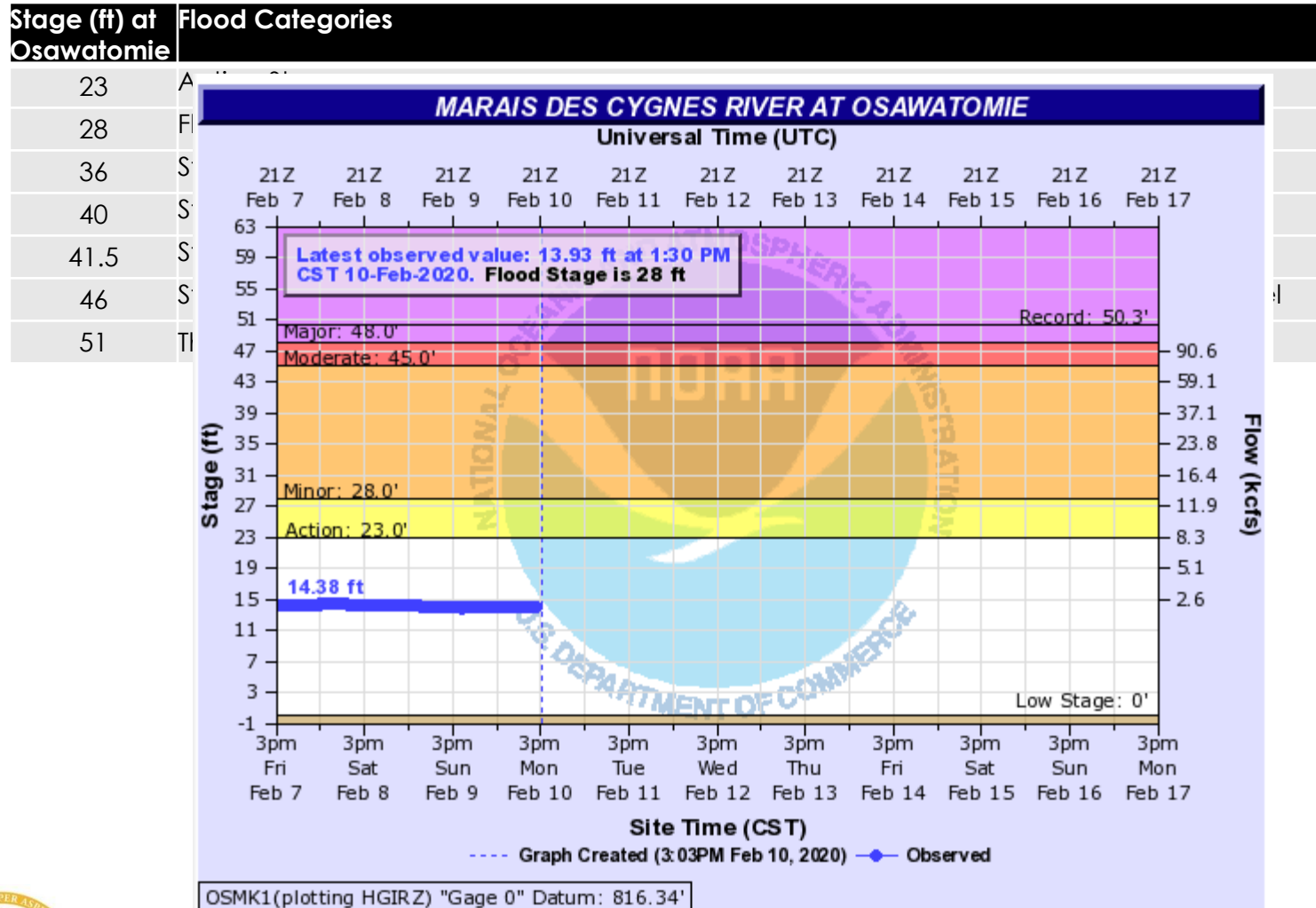
Results

Review Flood Forecasting Tables

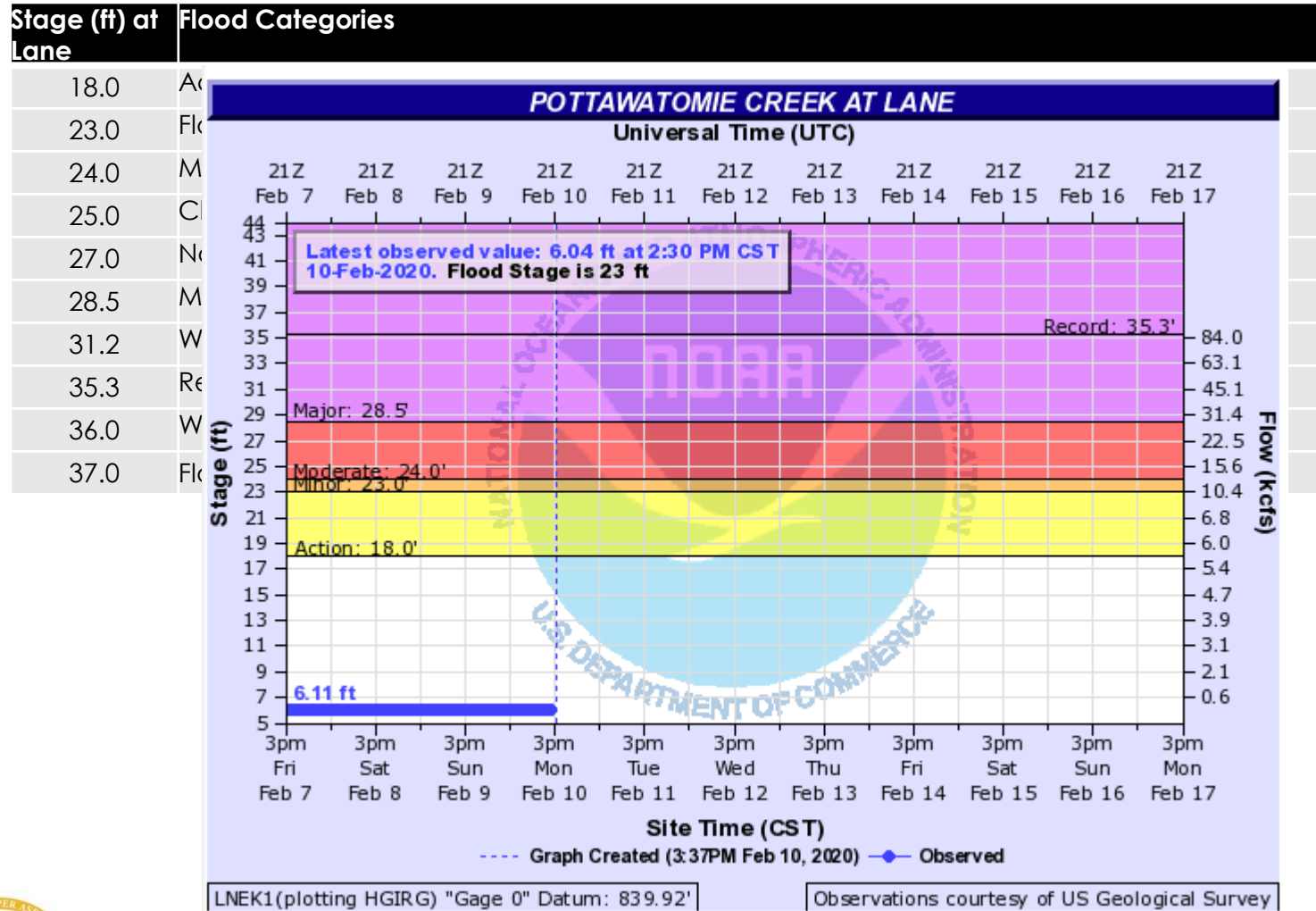
Review the Flood Forecasting Tables

- This is the community's opportunity to review the tables.
- Questions to consider:
 - What are the potential scenarios for the flood forecasting boundaries at Lane gage and Osawatomie gage?
 - What are the peak water surface elevations at railroad closure invert and when the peak will reach?
 - When will the water surface elevations reach the railroad closure invert elevation and what are the flows?

Scenario Analysis



Scenario Analysis



Reviewing the Tables

Peak WSE and Arrival Time (hours) at RR Closure

Appendix A: Peak water surface elevation (ft) and arrival time (hr) at railroad closure invert* for different stage combinations at Lane and Osawatimie gages

MDC Lane	Stage (ft)	23.0	28.0	36.0	40.0	41.5	43.0	46.0	51.0
Stage (ft)	Elevation (ft)	839.8	844.8	852.8	856.8	858.3	859.8	862.8	867.8
18.0	858.4	842.5 (3:20)	844.3 (3:00)	850.7 (2:35)	855.3 (2:10)	857.0 (2:25)	857.7*** (0:00)	862.2*** (0:00)	867.5*** (0:00)
23.0	863.4	847.8 (8:15)	848.4 (8:05)	851.8 (7:05)	855.6 (4:50)	857.3 (3:55)	858.9 (2:50)	862.3 (1:15)	
24.0	864.4	848.8 (9:20)	849.1 (9:00)	852.3 (8:00)	855.8 (5:40)	857.4 (4:30)	859.0 (3:30)	862.3 (1:15)	
25.0	865.4	850.1 (9:50)	850.4 (9:40)	852.7 (8:20)	856.0 (6:15)	857.6 (5:25)	859.1 (4:20)	862.5 (2:35)	
27.0	867.4	852.4 (9:30)	852.5 (9:20)	854.0 (8:25)	856.7 (7:05)	858.0 (6:25)	859.5 (5:25)	862.6 (2:55)	
27.5	867.9	853.3 (9:15)	853.4 (9:00)	854.7 (8:20)	857.1 (7:00)	858.3 (6:20)	859.7 (5:35)	862.8 (3:35)	
28.5	868.9	854.0 (9:00)	854.1 (8:45)	855.0 (8:20)	857.3 (7:05)	858.5 (6:25)	859.9 (5:45)	862.9 (3:40)	868.2 (0:40)
30.0	870.4	856.0 (8:25)	856.0 (8:15)	856.6 (7:55)	858.4 (7:15)	859.4 (6:45)	860.6 (6:00)	863.3 (4:05)	868.3 (1:15)
31.2	871.6	857.7** (8:00)		858.2 (7:30)	859.6 (6:55)	860.4 (6:30)	861.4 (5:55)	863.7 (4:25)	868.5 (1:45)
32.0	872.4	858.7** (7:05)		858.7 (7:25)	859.9 (6:50)	860.7 (6:30)	861.6 (5:50)	863.8 (4:25)	868.6 (1:50)
33.0	873.4	860.3** (7:05)		860.6 (6:50)	861.6 (6:10)	862.2 (5:50)	863.0 (5:30)	864.7 (4:20)	868.9 (2:05)
35.3	875.7	864.0** (5:35)		864.1 (5:35)	864.7 (5:25)	865.1 (5:30)	865.8 (4:45)	866.4 (3:15)	869.6 (1:50)
36.0	876.4	864.7** (5:40)		864.7 (5:30)	865.3 (5:10)	865.8 (5:35)	866.1 (4:05)	866.6 (3:10)	869.8 (1:55)
37.0	877.4	866.5** (5:35)		866.7 (5:35)	867.1 (4:35)	867.1 (4:00)	867.1 (3:35)	867.7 (3:20)	870.2 (2:05)
No flooding at the railroad closure		Water within 2.0 ft below railroad closure invert		Water overtops railroad closure invert		Water overtopping at railroad closure			

*Railroad closure invert elevation of 858.7 ft NAVD88 is stage 0.0 ft.

**Under conditions of high flow at Lane and low stage at Osawatimie, normal depth was used as downstream boundary condition.

***Under conditions of low flow at Lane and high stage at Osawatimie, the stage at Lane would be higher than expect. The water surface elevation at the flood start time was reported for these scenarios.

May 2019 Event

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Reviewing the Tables

Peak Stage and Arrival Time (hours) at RR Closure

Appendix B: Peak stage (ft) and arrival time (hr) at railroad closure invert* for different stage combinations at Lane and Osawatimie

MDC (ft) \ Lane (ft)	23.0	28.0	36.0	40.0	41.5	43.0	46.0	51.0
18.0	-16.2 (3:20)	-14.4 (3:00)	-8.0 (2:35)	-3.4 (2:10)	-1.7 (2:25)	0*** (0:00)	3.5*** (0:00)	8.8*** (0:00)
23.0	-10.9 (8:15)	-10.3 (8:05)	-6.9 (7:05)	-3.1 (4:50)	-1.4 (3:55)	0.2 (2:50)	3.6 (0:40)	
24.0	-9.9 (9:20)	-9.6 (9:00)	-6.5 (8:00)	-2.9 (5:40)	-1.3 (4:30)	0.3 (2:50)	3.6 (1:15)	
25.0	-8.6 (9:50)	-8.3 (9:40)	-6.1 (8:20)	-2.7 (6:15)	-1.2 (5:25)	0.4 (4:20)	3.8 (2:35)	
27.0	-6.3 (9:30)	-6.2 (9:20)	-4.7 (8:25)	-2.0 (7:05)	-0.7 (6:25)	0.8 (5:25)	3.9 (2:55)	
27.5	-5.4 (9:15)	-5.3 (9:00)	-4.0 (8:20)	-1.6 (7:00)	-0.4 (6:20)	1.0 (5:35)	4.1 (3:35)	
28.5	-4.7 (9:00)	-4.7 (8:45)	-3.7 (8:20)	-2.5 (7:05)	-0.2 (6:25)	1.2 (5:45)	4.2 (3:40)	9.3 (0:40)
30.0	-2.7 (8:25)	-2.7 (8:15)	-2.1 (7:55)	-0.3 (7:15)	0.7 (6:45)	1.9 (6:00)	4.6 (4:05)	9.6 (1:15)
31.2	-1.0** (8:00)	-0.5 (7:30)	0.9 (6:55)	1.7 (6:30)	2.7 (5:55)	5.0 (4:25)	9.8 (1:45)	
32.0	0.0** (7:05)	0.0 (7:25)	1.2 (6:50)	2.0 (6:30)	3.7 (5:50)	5.1 (4:25)	9.9 (1:50)	
33.0	1.6** (7:05)	1.9 (6:50)	2.9 (6:10)	3.5 (5:50)	4.3 (5:30)	6.0 (4:20)	10.2 (2:05)	
35.3	5.3** (5:50)	5.4 (5:35)	6.0 (5:25)	6.4 (5:30)	7.1 (4:45)	7.6 (3:15)	10.9 (1:50)	
36.0	6.0** (5:40)	6.0 (5:30)	6.6 (5:10)	7.0 (5:35)	7.4 (4:05)	7.9 (3:10)	11.1 (1:55)	
37.0	7.8** (5:35)	8.0 (5:35)	8.4 (4:35)	8.4 (4:00)	8.4 (3:35)	9.0 (3:20)	11.5 (2:05)	

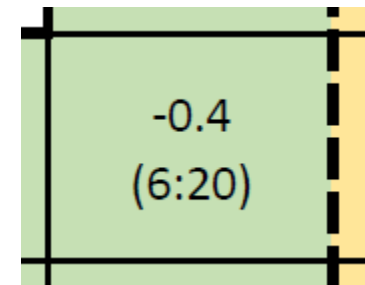
No flooding at the railroad closure | Water within 2.0 ft below railroad closure invert | Water overtops railroad closure invert | Levee overtopping at railroad closure

*Railroad closure invert elevation of 858.7 ft NAVD88 is stage 0.0 ft.

**Under conditions of high flow at Lane and low stage at Osawatimie, normal depth was used as downstream boundary condition.

***Under conditions of low flow at Lane and high stage at Osawatimie, the stage at Lane would be higher than expect. The water surface elevation at the flood start time was reported for these scenarios.

May 2019 Event



Reviewing the Tables

Flow and Arrival Time (hours) to RR Closure Invert

Appendix C: Pottawatomie Creek discharge (kcfs) and arrival time (hr) to reach the railroad closure invert* for different stage combination at Lane and Osawatomie gages

MDC Lane	Stage (ft)	23.0	28.0	36.0	40.0	41.5	43.0	46.0	51.0
Stage (ft)	Elevation (ft)	839.8	844.8	852.8	856.8	858.3	859.8	862.8	867.8
18.0	858.4						0.0*** (0 kcfs) (0:00)	3.5*** (0 kcfs) (0:00)	8.8*** (0 kcfs) (0:00)
28.0	868.4					0.0 (27 kcfs) (5:30)			
29.8	870.2				0.0 (36 kcfs) (6:50)				
31.3	871.7			0.0 (44 kcfs) (8:10)					
31.6	872.0	0.0** (46 kcfs) (8:25)							
No flooding at the railroad closure			Water within 2.0 ft below railroad closure invert		Water at railroad closure invert			Water above railroad closure invert	

*Railroad closure invert elevation of 858.7 ft NAVD88 is stage 0.0 ft.

**Under conditions of high flow at Lane and low stage at Osawatomie, normal depth was used as downstream boundary condition.

***Under conditions of low flow at Lane and high stage at Osawatomie, the stage at Lane would be higher than expect. The water surface elevation at the flood start time was reported for these scenarios.

Questions and Answers

Have We Answered
All Your Questions?

